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(54) **Optical signal power detection with signature bit pattern in WDM systems**

(57) The power of an optical signal ( $s_1$ ) travelling on a channel ( $\lambda_1$ ) of a WDM transmission system, is measured using a signature bit pattern ( $s_{BP1}$ ) which is inserted in the frame of the optical signal ( $s_1$ ). The power level of  $s_{BP1}$  is adjusted at the launching point to a predetermined ratio ( $m$ ) with the power of the optical signal. At a point of interest, the fiber is tapped and a fraction of

the tapped signal, that includes a corresponding fraction of  $s_{BP1}$ , is converted to an electrical signal. The fraction of  $s_{BP1}$  is extracted from the electrical signal and power of  $s_{BP1}$  is measured. This gives the optical power of  $s_1$  as ( $m$ ) is known and also the calibration constant for the respective channel ( $\lambda_1$ ) is known. The method can be applied for any and all channels of the WDM transmission system.

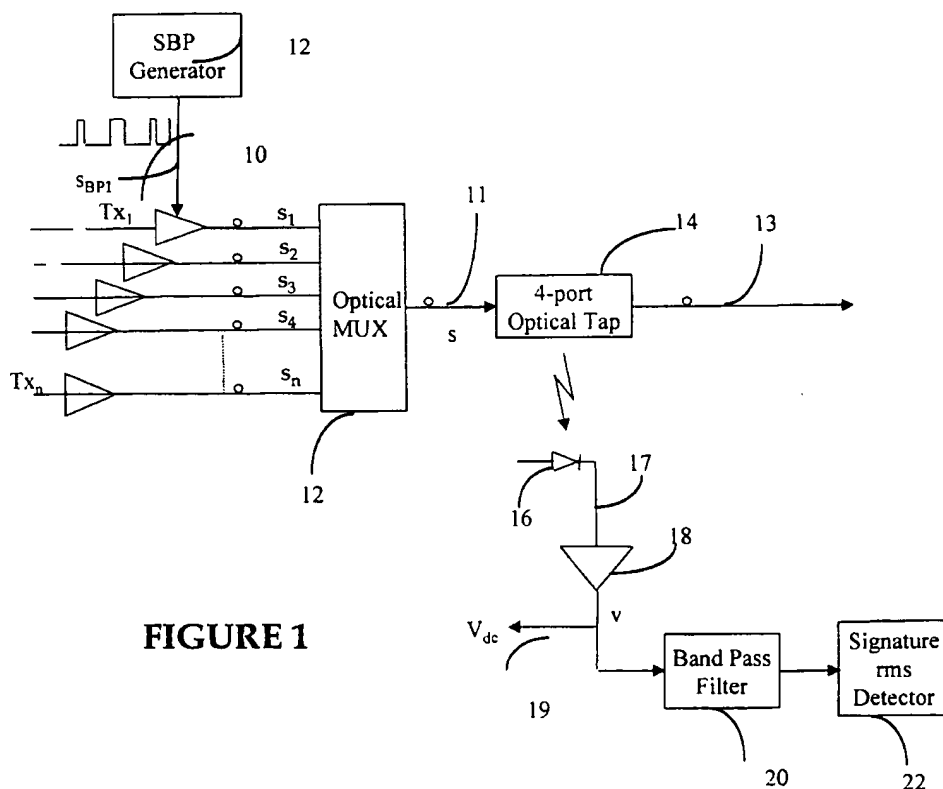


FIGURE 1

**Description****BACKGROUND OF THE INVENTION**5 **Field of the Invention**

[0001] This invention is directed to a method for monitoring the performance of optical WDM systems and in particular to an optical signal power detection method using a signature bit pattern.

10 **Background Art**

[0002] In optical transmission systems, various parameters such as power are measured to obtain information on the operating conditions of the transmission link. The fiber optic cables are tested by measuring the power losses associated with the light transmission, and thus, determine potential transmission errors.

15 [0003] In a WDM system, because different wavelengths of light have different attenuation characteristics, it is important to determine the attenuation of the fiber optic cable with respect to a specific wavelength of light used for a particular transmission channel. It is important to detect accurately the optical power of individual optical signals for many reasons, such as improved control of optical amplifiers, signal tracking at the optical layer, monitoring the accumulation of optical noise in a link with cascaded amplifiers, etc.

20 [0004] It is known to monitor the input and output of an optical amplifier in order to control the gain. To this end, fractions of the input and output signals are coupled out by taps (couplers) and detected by photodiodes. The electrical signals, recovered after this detection, are then used by the power monitor as needed. Since the power of the coupled out signal is very low in the case of digital systems, the power monitors required to detect and process this low signal are rather complex.

25 [0005] To date, the only other method for detecting the optical power of signals without using expensive optical filters is to amplitude modulate the optical signal to a controlled modulation depth with a signal (dither) unique to the respective transmission system. This method, disclosed in United States Patent No. 5, 513,029 by Kim Roberts, issued on April 30, 1996 and assigned to Northern Telecom Limited, requires additional optical components, such as an external modulator and optical attenuators, and also requires electronics and real time control software at the transmitter, to  
30 both apply the amplitude modulation and to detect it, in order to accurately control the modulation depth.

**SUMMARY OF THE INVENTION**

35 [0006] It is an object of the present invention to provide a method for detecting the optical power of a digital optical signal in the presence of other optical signals at different wavelengths, without using expensive fixed or tracking optical filters.

[0007] Accordingly, there is provided a method for measuring the power of an optical signal ( $s_1$ ) travelling on a first channel ( $\lambda_1$ ) of a WDM transmission system, comprising the steps of, generating a signature bit pattern ( $s_{BP1}$ ), adjusting the power level of the signature bit pattern to a predetermined ratio ( $m$ ) with the power of the optical signal, inserting  
40 the signature bit pattern ( $s_{BP1}$ ) into the frame of the optical signal ( $s_1$ ) and transmitting same along a span of transmission medium, measuring the power of the signature bit pattern ( $s_{BP1}$ ) at a point of interest on the span, and determining the optical power of the optical signal ( $s_1$ ) in the point of interest.

[0008] The advantage of this invention is that it provides a simple method for determining the optical power in a WDM system, whereby no additional electronics, expensive optical components and real time software are required at the  
45 transmitter side, resulting in considerable savings in circuit pack layout space, cost and development time.

**BRIEF DESCRIPTION OF THE DRAWINGS**

50 [0009] The foregoing and other objects, features and advantages of the invention will be apparent from the following more particular description of the preferred embodiment, as illustrated in the appended **Figure 1** which shows a block diagram of a WDM system according to the invention.

**DESCRIPTION OF THE PREFERRED EMBODIMENT**

55 [0010] For this invention, a unique signature bit pattern is inserted in a digital optical signal, where the rms (root mean square) of the signature bit pattern has inherently a fixed ratio to the optical power. Detecting the rms of this signature bit pattern means the optical power of the optical signal can be determined. As well, the optical power of the optical signals co-propagating along the same fiber span may be detected at the same time, when each optical signal

is given a unique signature pattern. The signature bit pattern for each co-propagating signal is designed to be detected independently from each other.

[0011] Figure 1 shows a block diagram of a WDM system using the signature bit patterns according to the invention. The WDM system of Figure 1 shows a plurality of optical signals  $s_1 - s_n$  propagating in the same direction. It is to be understood that the invention applies also to bidirectional optical WDM systems, such as for example to SONET/SDH 8-wavelength bidirectional systems.

[0012] Signals  $s_1 - s_n$  are multiplexed in an optical multiplexer 10 to obtain a multichannel signal  $s$  on fiber 12. A signature bit pattern, shown at  $s_{BP1}$ , is inserted into the frame of optical signal  $s_1$ . If we note the average optical power of  $s_1$  with ' $P_1$ ', the average optical power of  $s_{BP1}$  with ' $P_{BP1}$ ', and the ratio between the powers of  $s_{BP1}$  and  $s_1$  with ' $m$ ', we have the following relationship:

$$m = P_{BP1}/P_1 \text{ or, } P_{BP1} = m \times P_1 \quad (1)$$

[0013] As the signature bit pattern is inserted in the frame of the digital optical signal, ratio ' $m$ ' remains constant along the entire path. This is however true only if either the extinction ratio for the optical signal remains constant and known, or the extinction ratio is kept better than an acceptable amount.

[0014] The optical signal  $s_1$  with the signature bit pattern is carried by channel  $\lambda_1$  on fiber 12, together with signals  $s_2 - s_n$ . A tap monitor at some point of interest in the WDM system, noted 14 on Figure 1, taps fiber 12 and receives a fraction of signal  $s$ , which comprises a respective fraction of the optical signals  $s_1 - s_n$  for all channels  $\lambda_1 - \lambda_n$ . The tapped fraction is converted to an electrical signal, shown by reference numeral 19, by PIN diode 18 and then amplified by transimpedance amplifier 20.

[0015] The electrical signal  $v$  at the output of transimpedance amplifier 20 comprises an ac and a dc component. The dc voltage  $V_{dc}$  is a linear combination of the individual optical signal powers:

$$V_{dc} = a \times P_1 + b \times P_2 + c \times P_3 + \dots n \times P_n \quad (2)$$

where  $a, b, \dots n$  are known calibration constants for the respective transmission channel, and  $P_1 - P_n$  are the optical powers of the respective optical signals  $s_1 - s_n$ .

[0016] Signal  $v$  is filtered in a band pass filter 22 for extracting the frequencies of interest, which in this case are the component frequencies of the signature bit pattern  $s_{BP1}$ . A signature rms detector 24 detects the ' $rms_1$ ' of  $s_{BP1}$  independent from the interferences from the co-propagating optical signals. The signature rms detector may be realized either with an analog filter with peak detect circuitry, or with a super Nyquist sampling A/D converter and a DSP chip to implement a digital matched filter detection.

[0017] At the frequencies of interest, the power of the signature bit patterns for the other channels  $\lambda_2$  to  $\lambda_n$  is practically zero, by design, so that the measured  $rms_1$  gives  $P_{BP1}$  using the relation:

$$P_{BP1} = rms_1/a \quad (3)$$

where ' $a$ ' is the calibration constant for channel  $\lambda_1$ , known. The value of  $P_1$  can now be determined knowing  $m$ , which gives:

$$P_1 = rms_1 / m \times a \quad (4)$$

[0018] In a similar way, if the other signals  $s_2 - s_n$  have their own unique signature pattern, or analog dither, the optical power of these signals can be determined in the same way, as long as all the signal dithers are designed to be independently detected from each other, for example they are frequency division multiplexed.

[0019] An example of an implementation of the invention is the application of the signature bit pattern of the invention to determining the power of the bidirectional service optical channel (Bi-OSC). Bi-OSC is a service channel that is transmitted and terminated at each optical amplifier. This channel has a signalling rate of 9.72 Mb/s in each direction and is Manchester encoded in order to reduce its interference in the analog maintenance bandwidth (40 kHz) to acceptable levels.

[0020] The wavelength of the channel for one direction of transmission is selected in the red band and for the reverse direction, in the blue band. The frame of the signal transmitted on this channel has 2430 bits, 96 bits being used for

the signature. The average optical power of the Bi-OSC is also accounted for in order to make the average output control in the forward direction of transmission (i.e. the red band) and in the reverse direction of transmission (i.e. the blue band) more accurate by subtracting the power contribution from the respective OSC channels.

**[0021]** The signature bit pattern for the red channel is inserted on a frame by frame basis. After the Manchester encoding, the red OSC signature pattern is inserted in the following bit positions of the red OSC frame.

Table 1.

Red OSC signature bit pattern	
Bit Position	Red OSC signature block
1	1111 0011 1100 0110
401	0011 1100 1111 0110
801	0011 1100 1111 0110
1217	0000 1100 0011 1001
1617	1100 0011 0000 1001
2017	1100 0011 0000 1001

**[0022]** The spectrum of the red OSC signature bit pattern comprises odd multiples of 4kHz, namely 4kHz, 12kHz, 20kHz, etc. which makes it phase orthogonal to the AM dithers, SONET 8kHz tones and the blue signature bit pattern.

**[0023]** The minimum hamming distance between the first block and the other blocks within the frame is 8.

**[0024]** The signature bit pattern for the blue channel is inserted on a two consecutive frame by two consecutive frame basis. After the Manchester encoding, the blue OSC signature pattern is inserted in the following bit positions.

Table 2.

Blue OSC signature bit pattern		
Frame #	Bit Position	Red OSC signature block
First Frame	1	1111 0011 1100 0110
	401	0011 1100 1111 0110
	801	0011 1100 1111 0110
	1217	1100 0011 0000 1001
	1617	1100 0011 0000 1001
	2017	1100 0011 0000 1001
Second Frame	1	0000 1100 0011 1001
	401	1100 0011 0000 1001
	801	1100 0011 0000 1001
	1217	0011 1100 1111 0110
	1617	0011 1100 1111 0110
	2017	0011 1100 1111 0110

**[0025]** The spectrum of the blue OSC signature bit pattern are odd multiples of 2kHz, namely 2kHz, 16kHz, 10kHz, etc. which makes it phase orthogonal to the AM dithers, SONET 8kHz tones and the blue signature bit pattern.

**[0026]** The minimum hamming distance between the first block and the other blocks within the frame is 8.

**[0027]** While the invention has been described with reference to particular example embodiments, further modifications and improvements which will occur to those skilled in the art, may be made within the purview of the appended claims, without departing from the scope of the invention in its broader aspect.

## Claims

1. A method for measuring the power of an optical signal ( $s_1$ ) travelling on a first channel ( $\lambda_1$ ) of a WDM transmission system, comprising the steps of:

generating a signature bit pattern ( $s_{BP1}$ );

adjusting the power level of said signature bit pattern to a predetermined ratio ( $m$ ) with the power of said optical signal;

inserting said signature bit pattern ( $s_{BP1}$ ) into the frame of said optical signal ( $s_1$ ) and transmitting same along a span of transmission medium;

measuring the power of said signature bit pattern ( $s_{BP1}$ ) at a point of interest on said span; and

determining the optical power of said optical signal ( $s_1$ ) in said point of interest.

2. A method as claimed in claim 1, wherein said signature bit pattern ( $s_{BP1}$ ) is unique to said span.

3. A method as claimed in claim 1, wherein said step of inserting comprises providing the bits of said signature bit pattern ( $s_{BP1}$ ) in predetermined positions of the frame of said optical signal ( $s_1$ ) just before launching said signal on said fiber span.

4. A method as claimed in claim 3, further comprising:

providing a plurality of optical signals ( $s_i$ ), each for a respective transmission channel ( $\lambda_i$ ), where  $i \in [2, n]$ ; and

multiplexing said optical signal ( $s_1$ ), comprising said signature bit pattern ( $s_{BP1}$ ), with said optical signals ( $s_i$ ) into a multichannel signal ( $s$ ) and launching said multichannel signal ( $s$ ) on said span.

5. A method as claimed in claim 4, wherein said step of measuring the power of said signature bit pattern ( $s_{BP1}$ ) comprises:

taping a fraction of said multi-channel signal ( $s$ ) in said point of interest;

converting said fraction into an electrical signal ( $v$ );

filtering said electrical signal ( $v$ ) to pass a signature signal of a band comprising the frequency components of said signature bit pattern; and

measuring the root mean square  $rms_{SB1}$  value of said signature signal.

6. A method as claimed in claim 5, wherein said step of determining the optical power ( $P_1$ ) of said optical signal ( $s_1$ ) comprises applying said ratio ( $m$ ) to said  $rms_{SB1}$  value.

7. A method as claimed in claim 6, further comprising applying a correction factor ( $a$ ) to said ( $P_1$ ).

8. A method as claimed in claim 5, wherein measuring the root mean square  $rms_{SB1}$  value of said signature signal is performed with an analog filter with peak detect circuitry.

9. A method as claimed in claim 5, wherein said step of measuring the root mean square  $rms_{SB1}$  value of said signature signal comprises digital matched filter detection.

10. A method as claimed in claim 9, wherein said digital matched filter detection is performed with a super Nyquist sampling analog-to-digital converter and a digital signal processing unit.

11. A method as claimed in claim 4, wherein each of said optical signals ( $s_i$ ) comprises a respective signature bit pattern ( $s_{BPi}$ ) for detecting a respective, optical power ( $P_i$ ) of a restrictive optical signal ( $s_i$ ) in said point of interest.

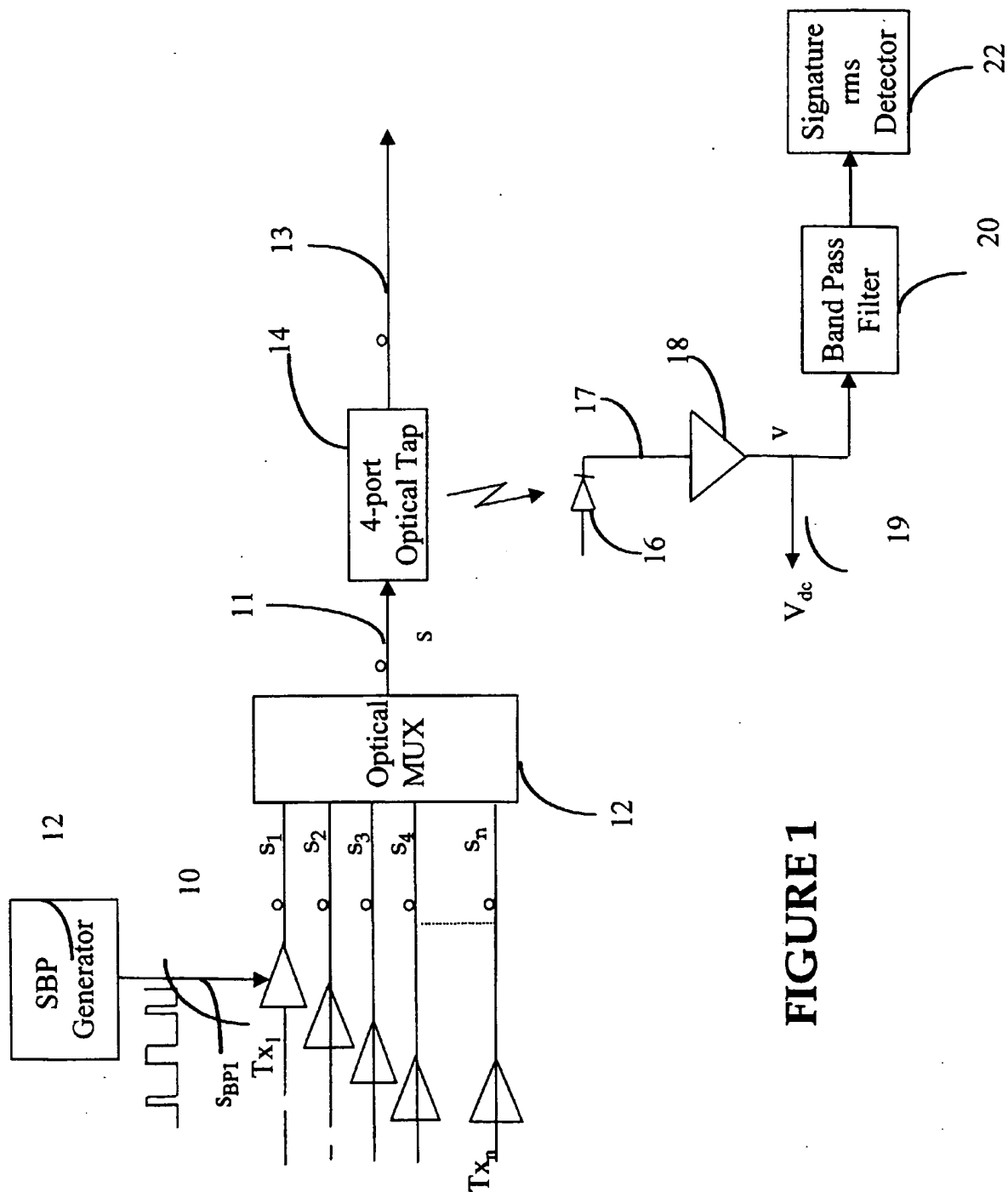


FIGURE 1